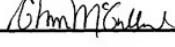


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<b>UTILITY PATENT APPLICATION TRANSMITTAL</b> (Only for new nonprovisional applications under 37 CFR 1.53(b))		Attorney Docket No. 198045US3
		First Inventor or Application Identifier Taku ICHIRYU
		Title FASTENING ARRANGEMENT FOR A SPLIT CASING

<b>APPLICATION ELEMENTS</b> See MPEP chapter 600 concerning utility patent application contents		ADDRESS TO: Assistant Commissioner for Patents Box Patent Application Washington, DC 20231
<p>1. <input checked="" type="checkbox"/> Fee Transmittal Form (e.g. PTO/SB/17) (Submit an original and a duplicate for fee processing)</p> <p>2. <input checked="" type="checkbox"/> Specification Total Pages <b>24</b></p> <p>3. <input checked="" type="checkbox"/> Drawing(s) (35 U.S.C. 113) Total Sheets <b>9</b> <b>(Formals)</b></p> <p>4. <input checked="" type="checkbox"/> Oath or Declaration Total Pages <b>3</b></p> <p>a. <input checked="" type="checkbox"/> Newly executed (original) <input type="checkbox"/> Copy from a prior application (37 C.F.R. §1.63(d)) (for continuation/divisional with box 15 completed)</p> <p>i. <input type="checkbox"/> <b>DELETION OF INVENTOR(S)</b> The entire disclosure of the prior application, from which a copy or a reference to such application is made, is being incorporated by reference herein.</p> <p>5. <input type="checkbox"/> Incorporation By Reference (usable if box 4B is checked) The entire disclosure of the prior application, from which a copy of the claims or disclosure is being incorporated by reference herein, is considered to be part of the disclosure of the accompanying application and is hereby incorporated by reference therein.</p>		<b>ACCOMPANYING APPLICATION PARTS</b>
<p>6. <input checked="" type="checkbox"/> Assignment Papers (cover sheet &amp; document(s))</p> <p>7. <input type="checkbox"/> 37 C.F.R. §3.73(b) Statement <input type="checkbox"/> Power of Attorney (when there is an assignee)</p> <p>8. <input type="checkbox"/> English Translation Document (if applicable)</p> <p>9. <input checked="" type="checkbox"/> Information Disclosure Statement (IDS)/PTO-1449 <input checked="" type="checkbox"/> Copies of IDS Citations (2)</p> <p>10. <input type="checkbox"/> Preliminary Amendment</p> <p>11. <input checked="" type="checkbox"/> White Advance Serial No. Postcard</p> <p>12. <input type="checkbox"/> Small Entity Statement(s) <input type="checkbox"/> Statement filed in prior application. Status still proper and desired.</p> <p>13. <input checked="" type="checkbox"/> Certified Copy of Priority Document(s) (1) (if foreign priority is claimed)</p> <p>14. <input checked="" type="checkbox"/> Other: Notice of Priority</p>		
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## IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

INVENTOR(S) Taku ICHIRYU

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FASTENING ARRANGEMENT FOR A SPLIT CASING

## BACKGROUND OF THE INVENTION

## 5 1. Field of the Invention

The present invention relates to a fastening arrangement for a split casing. More specifically, the present invention relates to a fastening arrangement which is especially advantageous, for example, when used 10 for forming casings of hydraulic machines, such as turbines and compressors, as flangeless casings.

## 15 2. Description of the Related Art

A horizontally split type casing construction is commonly used for casings of turbines and compressors. In the horizontally split type casing construction, a casing is divided into two segments by a plane including a center axis thereof. Usually, each casing segment (casing half) is provided with plate-like flanges having a relatively large thickness at joint portions of the casing. The casing halves are coupled to each other by joining and fastening the flanges together by fastening 20 bolts.

Fig. 7 illustrates a fastening arrangement of a conventional horizontally split type casing having flanges. Fig. 7 shows a section perpendicular to an axis 25 of the casing.

In Fig. 7, reference numeral 100 designates a casing consists of two casing halves 110a and 120a. 110b and 120b designate flanges formed at the joint portions 30 of the casing halves 110a and 120a. The flanges 110b and 120b are fastened together by a plurality of fastening bolts 115. Each of the fastening bolts is provided with a bolt head 115d at one end thereof and a screw thread 115a at the other end thereof. Threaded bolt holes 120c which engage the screw threads 115a of the 35 bolts 115 are provided on the flange 120b of one of the casing halves 120a. Further, the flange 110b of the

other casing half 110a is provided with bolt holes 110c. In order to join two casing halves 110a and 120a, the fastening bolts 115 are inserted into the bolt holes 110c of the flanges 110b of the casing half 110a and the threads 115a of the bolt 115 are screwed into the threaded bolt holes 120c on the flanges 120b of the casing half 120a until the bolt heads 115d are pressed against the upper face of the flange 110b. By tightening the fastening bolt 115, flanges 110b and 120b are firmly 5 pressed against each other by the bolt heads 115d and the screw threads 115a of the bolt 115. In this condition, the tensile force is generated on the shaft of the bolt by tightening the bolt 115. The reaction force of the shaft tensile force is exerted on the upper face of the 10 flange 110b through the bolt heads 115d and also on the screw threads of the threaded bolt holes 120c in the opposite direction. Due to these reaction forces, the 15 flanges 110b and 120b are pressed against each other.

However, in some cases, problems occur when the 20 fastening arrangement using the flanges as illustrated in Fig. 7 is used for the horizontally split type casings of hydraulic machines such as turbines or compressors.

In hydraulic machines having rotors, the 25 casings containing rotors must have strictly circular cross sections especially at the inner peripheries. However, in the turbines and compressors, since the temperature of the fluid passing through the casings is high, the temperature of the respective portions of the casings becomes high. If the temperature of the casing 30 wall varies in the respective portions, a large thermal stress is generated by the difference in the amount of the thermal expansion of the respective portions of the casing. When a large thermal stress is generated, the casing tends to deform and concentricity of the cross 35 section of the casing cannot be maintained. Further, in the turbines and compressors, the temperature of the fluid passing through the machines changes considerably

due to a change in the operating load. In this case, if  
the casing is provided with flanges having a thickness  
larger than other portions of the casing, the change in  
the temperature of the flanges is late compared with the  
other portions. This causes a large temperature  
difference between the flanges and other casing portions  
when the rate of the change in the temperature of the  
fluid in the casing is high. Therefore, if the casing is  
provided with flange having a large thickness, distortion  
of the casing may occur when the temperature of the fluid  
changes.

In turbines and compressors, rotors rotating at  
high speed are accommodated in the casings. Therefore,  
if distortion of the casing occurs, the outer periphery  
15 of the rotor (such as the tips of the turbine blades)  
contact with the inner periphery of the casing. This may  
cause damage to the machine. It is true that the contact  
between the rotor and the casing can be avoided even in  
this case if the clearance between the tips of the  
20 turbine blades and the inner periphery of the casing is  
set at a relatively large value. However, in the  
hydraulic machines such as turbines and compressors,  
since the efficiency of the machine decreases as the tip  
clearance becomes larger, it is not practical to set the  
tip clearance to a large value.

In order to solve the problems explained above,  
a flangeless casing which eliminates the use of the  
flanges is used in some cases for the horizontal split  
type casing. The flangeless casing is a casing which  
30 does not use flanges such as shown in Fig. 7 for joining  
the casing halves. Fig. 8 is a sectional view similar to  
Fig. 7 which illustrates a typical fastening arrangement  
of a flangeless casing.

As can be seen from Fig. 8, the casing  
35 halves 210a and 220a of the flangeless casing 200 have  
semi-circular cross sections without flanges at joining  
faces. The bolt holes 210c and 220c for fastening

bolts 215 are drilled in the tangential direction in the walls of the casing halves 210a and 220a. Spot facings are formed on the upper ends of the bolt holes 210c in order to obtain a close contact between the surfaces of the casing half 210a around the bolt holes 210c and the bolt heads 215d of the fastening bolts 215.

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In the flangeless casings as shown in Fig. 8, since the flanges having a large thickness are not used, a non-uniformity of the thickness of the casing is smaller compared with the flanged casings and the distortion of the casing due to the change in the temperature of the fluid also becomes smaller. However, even in the flangeless casing in Fig. 8, the problems similar to the flanged casings may occur when the pressure or the temperature of the internal fluid is high.

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In the flangeless casings in Fig. 8, since the spot facings 210d are provided, the diameters of the bolt holes 210c above the spot facings are required to be the same as the diameters of the spot facings 210d. Therefore, the diameter of the bolt holes 210c becomes much larger than the minimum diameter required for allowing the bolt 215 to pass through. This means that a larger amount of metal must be removed from the walls of the casing half 210a and reduced wall thickness portions are formed by the bolt holes 210c. As illustrated in Fig. 8 the wall thickness becomes the smallest ( $T_1$  in Fig. 8) at the portion where the spot facings are formed.

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Fig. 9 schematically shows a section of the wall of the casing half 210a around the spot facings 210d taken along the line A-A in Fig. 8. As can be seen from Fig. 9, the wall is cut off in a cylindrical shape around the spot facings 210d and only a solid metal in the shape of the hatched area is remained. The average wall thickness of the portions shown by the hatched area is represented by  $T_2$  in Fig. 9. In other words, the effective wall thickness of the casing around the spot

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facings is reduced to a substantially small value  $T_2$  when the spot facings are formed. Therefore, in the flangeless casing in Fig. 8, reduced wall thickness portions are formed in the casing 210a by the spot facings 210d. Since the distortion of the casing occurs at these reduced wall thickness portions when the internal pressure or temperature of the casing is high, problems similar to those of the flanged casing of Fig. 7 occur.

In order to prevent the formation of the reduced wall thickness portions, it is necessary to reduce the diameters  $d$  (Fig. 8) of the spot facings 210d. However, practically it is not possible to reduce the diameter of the spot facing beyond some limit for the reasons explained below.

During the operation of the hydraulic machines, a large shaft tensile force are required for the fastening bolts in order to hold the casing halves together against the force generated by the internal fluid pressure and thermal stress exerting on the casing halves in a direction separating the casing halves from each other.

This means that a large force must be transferred from the fastening bolts to the casing 210a through the contacts between the bolt heads 215d and the spot facings 210d. Generally, the fastening bolts are made of a material having a high strength such as a high tension alloy. On the other hand, usually, a material having a high strength are not used for the casing halves in order to facilitate machining of the casing (such as cutting and, if required, welding) and to obtain a high resistance to a low frequency fatigue. Therefore, the maximum value of the contact pressure between the bolt heads and the casing is limited by the material used for the casing. Consequently, the diameter of the spot facing must be sufficiently large in order to reduce the contact pressure between the bolt head and the casing to

within the allowable limit determined by the material of the casing while maintaining a sufficiently large shaft tensile force of the fastening bolt. Thus, it is practically difficult to reduce the diameter of the spot facings in order to increase the effective wall thickness of the casing around the spot facings.

Further, it is preferable to dispose the fastening bolts at a smaller interval around the casing in order to obtain a large and uniform tightening force around the casing. However, since a large diameter is required for the spot facings, it is difficult to reduce the distance between the bolt holes 210c. A sufficiently large and uniform tightening force of the casing halves cannot be obtained in some cases in the flangeless casing in Fig. 8.

#### SUMMARY OF THE INVENTION

In view of the problems in the related art as set forth above, the objects of the present invention is to provide a fastening arrangement of a split casing capable of reducing the interval between the fastening bolts in order to obtain a large and uniform tightening force of the casing while maintaining a sufficiently large wall thickness of the casing.

The object as set forth above is achieved by a fastening arrangement for a split casing, according to the present invention, in which a casing is assembled by fastening a plurality of casing segments, comprising a first and a second casing segments assembled together by joining joint faces of the respective casing segments, the first and second casing segments are provided with bolt holes in such a manner that the bolt hole of the first casing segment and the bolt hole of the second casing segment align with each other and, when the first and the second casing segments are assembled together, form a continuous bolt hole crossing the joint faces and extending in both casing segments and, at least the bolt hole in the first casing segment is provided with an

internal screw thread, a sleeve having an external screw  
thread and being fitted into the bolt hole of the first  
casing segment by engaging the external screw thread of  
the sleeve with the internal screw thread of the bolt  
5 hole of the first casing segment and a fastening bolt  
provided with fastening means and passing through the  
bolt hole of the first casing segment and the sleeve  
therein, wherein the fastening means abuts an end of the  
sleeve opposite to the joint face and, when a tensile  
10 force is exerted on the fastening bolt at the portion  
between the fastening means and the second casing  
segments, the tensile force is first transferred from the  
fastening bolt to the sleeve through the abutment of the  
fastening means and the end face of the sleeve, then  
15 transferred from the sleeve to the first casing segment  
through the engagement of the external screw thread of  
the sleeve and the internal screw thread of the bolt hole  
and generates a fastening force for pressing the first  
casing segment against the second casing segment.

20 According to this aspect of the present invention,  
the fastening bolt does not directly contact the first  
casing segment. The shaft tensile force is transferred  
to the first casing segments through the sleeve. Since  
the sleeve can be made of a material separate from the  
25 casing segments, a material similar to that of the  
fastening bolt, i.e. a material having a high strength  
can be used for the sleeve. Therefore, the allowable  
maximum contact pressure between the fastening element  
and the end face of the sleeve can be largely increased.  
30 Thus, the contact area of the end face of the sleeve and  
the fastening element (i.e., the outer diameter of the  
sleeve) can be largely reduced without reducing the  
fastening force of the casing segments. Since this makes  
it possible to reduce the diameter of the bolt holes, the  
35 effective wall thickness of the casing can be increased  
and the interval between the fastening bolts can be  
reduced.

According to another aspect of the present invention, there is provided a fastening arrangement for a horizontally split type casing for a hydraulic machine in which the casing of the hydraulic machine is assembled by fastening two casing halves, comprising a first and a second casing halves assembled together by joining joint faces of the respective casing halves, the first and second casing halves are provided with bolt holes in such a manner that the bolt hole of the first casing half and the bolt hole of the second casing half align with each other and, when the first and the second casing halves are assembled together, form a continuous bolt hole crossing the joint faces and extending in both casing halves, the bolt holes in the first and the second casing halves are provided with internal screw threads, a sleeve having an external screw thread and being fitted into the bolt hole of the first casing half by engaging the external screw thread of the sleeve with the internal screw thread of the bolt hole of the first casing half, a fastening bolt provided with an external screw thread at one end for engaging the internal screw thread of the bolt hole in the second casing half and fastening means at the portion apart from the external screw thread, the fastening bolt passing through the bolt hole of the first casing half and the sleeve therein, wherein the fastening means abuts an end of the sleeve opposite to the joint face when the fastening bolt is screwed into the bolt hole in the second casing half, thereby a tensile force generated in the fastening bolt by screwing the fastening bolt into the bolt hole in the second casing half is first transferred from the fastening bolt to the sleeve through the abutment of the fastening means and the end face of the sleeve, then transferred from the sleeve to the first casing segment through the engagement of the external screw thread of the sleeve and internal screw thread of the bolt hole in the first casing half and generates a fastening force for pressing the first casing

half against the second casing half.

According to this aspect of the present invention, a casing of a hydraulic machine such as a turbine, a compressor or a pump is constructed as a horizontally split type casing. Also in this aspect of the invention, the shaft tensile force of the fastening bolt is transferred to the upper casing through the sleeve in order to increase the contact pressure between the end face of the sleeve and the fastening element. Since the effective wall thickness of the casing can be increased and the interval of the fastening bolts can be reduced, the casing halves are fastened together rigidly even though a high internal pressure and a high temperature is exerted on the casing of the hydraulic machine.

15            BRIEF DESCRIPTION OF THE DRAWINGS

The present invention will be better understood from the description, as set forth hereinafter, with reference to the accompanying drawings in which:

20            Fig. 1 is a sectional view illustrating an embodiment of a fastening arrangement for a flangeless casing according to the present invention;

Fig. 2 is an enlarged view of the portion II in Fig. 1;

25            Figs. 3A schematically illustrates the thickness of the casing at spot facings according to the related art in Fig. 8;

Fig. 3B schematically illustrates the thickness of the casing at spot facings according to the embodiment in Fig. 1;

30            Fig. 4 is a sectional view similar to Fig. 1 illustrating a second embodiment of the present invention;

Fig. 5 is a sectional view similar to Fig. 1 illustrating a third embodiment of the present invention;

35            Fig. 6 is a sectional view similar to Fig. 1 illustrating a fourth embodiment of the present invention;

Fig. 7 is a sectional view illustrating a typical fastening arrangement for a horizontally split type flanged casing;

5 Fig. 8 is a sectional view similar to Fig. 7 illustrating a conventional fastening arrangement for a horizontally split type flangeless casing; and

Fig. 9 is a sectional view taken along the line A-A in Fig. 8.

#### DESCRIPTION OF THE PREFERRED EMBODIMENT

10 Hereinafter, embodiments of a fastening arrangement for a flangeless casing according to the present invention will be explained with reference to Figs. 1 through 6.

##### (1) First embodiment

15 Fig. 1 illustrates a first embodiment of a fastening arrangement for a flangeless casing according to the present invention.

20 Fig. 1 is a sectional view of a casing of a gas turbine taken along the plane perpendicular to the center axis. The casing 10 of the gas turbine in Fig. 1 is constructed as a horizontally split type flangeless casing. More specifically the casing 10 in Fig. 1 is a cylindrical shape and split into two casing halves 1 and 2 by a plane including the center axis. The casing 25 half 1 (hereinafter referred to as the "upper casing") and the casing half 2 (hereinafter referred to as the "lower casing") are coupled by joining joint faces 3 and fastened to each other firmly.

30 In Fig. 1, reference numeral 5 designates a plurality of fastening bolts for fastening the upper casing 1 and lower casing 2 together. In this embodiment, a screw thread 5a is formed at lower end portion of each fastening bolt 5. The fastening bolts 5 pass through bolt holes 7 drilled in the upper casing 1 perpendicularly to the joint face 3 and the screw 35 threads 5a at the end thereof are screwed into threaded holes 5b formed on the joint faces 3 of the lower

casing 2. In this embodiment, the lengths of the bolts 5 are determined in such a manner that the upper end portions of the respective fastenings bolts 5 protrude from the bolt holes 7 of the upper casing 1 when the bolts 5 are tightened. The protruding ends of the fastening bolts 5 are formed as polygonal heads 5d to facilitate tightening the bolts 5 by a tightening tool such as a wrench.

Fig. 2 is an enlarged view of the portion indicated by II in Fig. 1. As can be seen from Fig. 2, an internal screw thread 9a is formed on the inner surface of the bolt hole 7 near the joint face 3. A cylindrical sleeve 11 having external thread 9b which engages the internal thread 9a is fitted in the bolt hole 7 by screwing the sleeve 11 into the bolt hole 7. When the sleeve 9 is fitted into the bolt hole 7, a clearance is formed between the lower end 11b of the sleeve 11 and the joint face 3 in order to avoid the contact between the lower end 11b of the sleeve 11 and the joint face 3 of the lower casing 2 when the fastening bolt 5 is fully tightened.

An enlarged diameter portion 5c is formed on the shaft portion of the fastening bolt 5 at the portion located inside of the bolt hole 7 when the bolt 5 is tightened. The diameter of the enlarged diameter portion 5c is slightly smaller than the diameter of the bolt hole 7. When the fastening bolt 5 is screwed into the threaded hole 5b of the lower casing 2, the lower face of the enlarged diameter portion 5c is pressed against the upper end face 11a of the sleeve 11. Therefore, when the fastening bolt 5 is further tightened, a tensile force is generated in the shaft portion of the fastening bolt 5. The reaction force of this shaft tensile force is transferred from the enlarged diameter portion 5c to the upper end face 11a of the sleeve 11 and a downward force is exerted on the sleeve 11. Since the external thread 9b of the sleeve 11

engages the internal thread 9a of the bolt hole 7, the downward force exerted on the sleeve 11 is received by the upper casing 1. Thus, the shaft tensile force of the fastening bolt 5 is converted to a tightening force which presses the upper casing 1 against the lower casing 2.

As explained above, the tightening force of the casing 10 in this embodiment is transferred to the upper casing 1 through the engagement between the thread 9b of the sleeve 11 and the thread 9a of the bolt hole 7 and to the lower casing 2 through the engagement between the thread 5a of the fastening bolt 5 and the thread of the threaded hole 5b.

In this embodiment, materials having a relatively low strength such as a carbon steel for boilers and pressure vessels (for example, Japanese industrial standard (JIS) SB410) or a cast steel for high temperature and high pressure (for example, JIS SCPH32) are used for the upper casing 1 and lower casing 2 to facilitate machining of the upper and lower casings. On the other hand, a material having a high strength, such as alloy steel bolting material (JIS SNB7) or heat resisting steel (JIS SUH616) is used for the fastening bolts 5 in order to obtain a large tightening force of the casing 10. Therefore, if the conventional fastening arrangement in which the bolt heads of the fastening bolts directly contact the upper casing is used, the maximum allowable contact pressure between the bolt heads and the casing is limited by the strength of the material used for casing. Thus, as explained before, spot facings having large diameters are required for casing in order to lower the contact pressure between the bolt heads and the casing. This causes the problems explained before, i.e., a smaller wall thickness of the casing at the spot facings and a larger intervals of the fastening bolts.

These problems are solved by inserting the cylindrical sleeve 11 made of a high strength material similar to that of the fastening bolts 5 (for example,

JIS SUH616 or an aluminum chromium molybdenum steel such as JIS SACM645) into the bolt hole 7. The enlarged diameter portion 5c of the fastening bolt 5 abuts the upper end face 11a of the sleeve 11 in this embodiment.

5 However, the sleeve 11 in this embodiment is made of a high strength material similar to that of the fastening bolt 5. Therefore, the allowable contact pressure between the enlarged diameter portion 5c and the upper end face 11a of the sleeve is much higher than that in the case where the bolt head of the fastening bolt 5 directly contacts the upper casing 2. Consequently, the contact pressure can be set at a higher value in order to reduce the contact area between the enlarged diameter portion 5c and the upper end face 11a of the sleeve 11.

10 Thus, the outer diameters of the enlarged portion 5c of the bolt 5 and the sleeve can be set at a value smaller than the diameter of the spot facing required in the case where the bolt head directly contacts the upper casing.

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In this embodiment, sleeve 11 is secured to the upper casing 1 through the screw threads 9a and 9b. However, since the number of the threads of the screw threads 9a and 9b can be determined arbitrarily, the contact pressure between the threads 9a and 9b and shearing stresses exerted thereon can be easily adjusted to values lower than the maximum allowable values. Therefore, problems concerning the strength of the thread do not occur in this embodiment.

The effect of the fastening arrangement in the present embodiment in the reduction of the diameter of the bolt hole 7 compared with the diameter of spot facing 210d in Fig. 8 will be explained below in detail using actual numerical values.

Assuming that a JIS M48 Allen screw is used for the fastening bolt 115 in the conventional fastening arrangement of Fig. 8, the outer diameter of the bolt head 215 becomes 78 mm. Consequently, a minimum 78 mm diameter (shown by d in Fig. 8) is required for the spot

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facing 210d.

On the other hand, when JIS M48 screw threads are used for the threads 5a and 5b in the fastening arrangement in Figs. 1 and 2, the outer diameter of the thread 5a of the fastening bolt 5 is 48 mm. Since the inner diameter (DIN in Fig. 2) must be slightly larger than the outer diameter of the thread 5a of the bolt 5 (i.e., 48 mm), the inner diameter DIN of the sleeve 11 is set at, for example, about 49 mm.

The diameter DB of the shaft of the bolt 5 is determined in such a manner that the tensile stress exerted on the shaft when the fastening bolt 5 is fully tightened is less than the maximum allowable tensile stress of the bolt material and, in this embodiment, the shaft diameter DB is set at 41 mm.

When the sleeve 11 is made of the material the same as that of the fastening bolt, the contact pressure between the enlarged diameter portion 5c of the bolt 5 and the upper end face 11a of the sleeve is sufficiently lower than the maximum allowable contact pressure if the contact pressure is set at a value less than the tensile stress of the shaft of the bolt 5. Therefore, the minimum required area of the upper end face 11a of the sleeve 11 (i.e., the area of the annular cross section of the sleeve 11) is the same as the cross section area of the shaft portion of the fastening bolt 5.

Since the diameter of the shaft portion of the fastening bolt 5 is DB, the cross sectional area of the shaft portion is expressed by  $(\pi/4) \times (DB)^2$ . Further, assuming that the outer diameter of the sleeve 11 is DOUT, the cross sectional area of the sleeve 11 is expressed by  $(\pi/4) \times ((DOUT)^2 - (DIN)^2)$ .

Since the cross sectional area of the sleeve 11 must be larger than or equal to the cross sectional area of the shaft portion of the bolt 5, the following relationship is obtained.

$$(\pi/4) \times ((DOUT)^2 - (DIN)^2) \geq (\pi/4) \times (DB)^2$$

Therefore, the required value of DOUT is

$$DOUT \geq ((DIN)^2 + (DB)^2)^{1/2}$$

Since DIN = 49 mm and DB = 41 mm in this embodiment, the minimum value of the outer diameter DOUT of the sleeve 11 becomes about 64 mm.

As can be seen from Fig. 2, the outer diameter DOUT of the sleeve 11 is the same as the minor diameter of the thread 9a (i.e., the diameter of the root of the thread 9a). According to the Japanese industrial standard (JIS), M68 or M72 threads have minor diameters about 64 mm. More precisely, JIS M68 thread has a minor diameter of 61.5 mm and JIS M72 thread has a minor diameter of 66 mm. Therefore, even if a larger size thread (i.e., JIS M72) is used, the outer diameter DOUT of the sleeve 11 is 66 mm. Since the diameter of the bolt hole 7 is the nearly the same as the outer diameter DOUT of the sleeve 11, the diameter of the bolt hole 7 in this embodiment is, at maximum, 66 mm. This diameter of the bolt hole 7 (66 mm) is substantially smaller than the diameter of the spot facing 210d (78 mm) in the conventional fastening arrangement in Fig. 8.

Figs. 3A and 3B show the comparison of the minimum wall thickness of the casing in the present embodiment (Fig. 3B) and the conventional fastening arrangement (Fig. 3A) based on the above calculated values. As can be seen from Figs. 3A and 3B, the minimum wall thickness in the present embodiment increases about 12 mm (= 78 - 66 mm) compared with the conventional fastening arrangement in Fig. 8. Further, it will be understood from Figs. 3A and 3B that the sectional area of the casing wall (the hatched area in Figs. 3A and 3B), which determines the magnitude of flexural rigidity of the casing wall, significantly increases in the present embodiment.

Further, though Figs. 3A and 3B show the case where the interval of the fastening bolt (the bolt pitch) is the same, it will be understood that the bolt pitch

can be reduced by maximum of 12 mm in the present embodiment in order to increase the tightening force of the casing.

5           (2) Second embodiment

Fig. 4 is a sectional view similar to Fig. 1 illustrating a second embodiment of the present invention. In Fig. 4, the reference numerals the same as those in Fig. 1 designate similar elements.

In this embodiment, a cylindrical sleeve similar to that in the first embodiment is used. However, although the sleeve 11 in the first embodiment is screwed into the bolt hole 7 from the joint face 3 side thereof, the sleeve 11 in this embodiment is screwed into the bolt hole 7 from the side thereof opposite to the joint face 3 and fitted inside the upper portion of the bolt hole 7. Further, the upper portion of the sleeve 11 protrudes from the bolt hole 7.

In this embodiment, an ordinary Allen screw the same as that in Fig. 8 is used in this embodiment. The diameter of the bolt head of an Allen screw is larger than the required diameter of the sleeve 11 as explained in the previous embodiment. Therefore, in order to avoid an increase in the diameter of the bolt hole 7 due to the large bolt head of the fastening bolt 5, the bolt head 5d is received by a flange 11f formed at the upper end of the sleeve 11 outside of the bolt hole 7 in this embodiment. The bolt head 5d in this embodiment acts as the fastening element similar to the enlarged diameter portion 5c of the first embodiment.

30           (3) Third embodiment

Fig. 5 is sectional view similar to Fig. 1 but illustrating a third embodiment of the present invention. In Fig. 5, the reference numerals the same as those in Figs. 1 and 2 designate similar elements.

35           In this embodiment, similar to the first embodiment, the sleeve 11 is screwed into the bolt hole 7 from the joint face 3 side. However, the shape of the

bolt hole 7 in this embodiment is different from that of the first embodiment. Namely, the diameter of the bolt hole 7, is enlarged at the lower portion thereof in order to accommodate the sleeve 11 and the diameter of the bolt hole 7 at the upper portion thereof is reduced to a value slightly larger than the diameter of the shaft portion 5s of the fastening bolt 5.

In contrast with the first embodiment, in order to fastening the casing 10, the fastening bolt 5 is first inserted into the bolt hole 7 from the joint face 3 side, then, the sleeve 11 is screwed into the bolt hole 7 from the joint face 3 side in such a manner that the enlarged diameter portion 5c of the bolt 5 remains in the bolt hole 7 above the sleeve 11. In this condition, the upper casing 1 and the lower casing 2 are joined together by abutting the joint faces 3 and the bolt 5 is screwed into the threaded hole 5b in the lower casing 2.

Since the diameter of the upper portion of the bolt hole 7 is reduced in this embodiment, the flexural rigidity of the casing wall is further increased compared with the first and the second embodiments. The flexural rigidity of the casing wall increases as the geometric moment of inertia (the second moment of area) around the neutral axis E of deflection becomes larger. The neutral axis E of deflection in this case is a center line of the wall thickness of the casing (Fig. 5). Therefore, when the distance between a void such as a bolt hole 7 and the neutral axis E becomes larger, the geometric moment of inertia around the neutral axis becomes smaller and, thereby, the flexural rigidity of the casing wall largely decreases.

In this embodiment, though the diameter of the lower portion (the portion A in Fig. 5) of the bolt hole 7, where the neutral axis E intersects the bolt hole, has a larger diameter, the diameter of the upper portion (the portion B in Fig. 5), where the distance between the neutral axis E and bolt hole 7 increases, is

reduced. Since the lower portion B is substantially on the neutral axis E, this portion does not substantially affect the geometric moment of inertia even though the diameter thereof is large. Further, although the  
5 distance D between the neutral axis E and the upper portion B of the bolt hole 7 is relatively large, the decrease in the geometric moment of inertia is minimized in this embodiment since the diameter of the upper portion B of the bolt hole 7 is reduced.

10 Thus, according to the present embodiment, the flexural rigidity of the casing wall is further increased by changing the diameter of the bolt hole 7 according to the distance of the respective portions of the bolt hole from the neutral axis E of deflection.

15 (4) Fourth embodiment

Fig. 6 is a sectional view similar to Fig. 1 illustrating a fourth embodiment of the present invention. In Fig. 6, reference numerals the same as those in Figs. 1 and 2 designate similar elements.

20 Opposite to the previous embodiments, the screw threads 5b which engages the thread 5a of the fastening bolt 5 is formed on the inner surface of the bolt hole 7 in the upper casing 1 and the threaded hole 9b which engages with the sleeve 11 is formed in the lower casing 2 in this embodiment. Further, the enlarged diameter portion 5c is disposed on the lower end of the fastening bolt 5 and the thread 5a which engages the thread 5b of the bolt hole 7 is disposed at the middle of the shaft portion of the bolt 5.

25 30 When tightening the casing 10, the enlarged diameter portion 5c at the lower end of the fastening bolt 5 is first inserted into the threaded hole 9b in the lower casing 2 from the joint face 3 side, then the sleeve 11 is screwed into the threaded hole 9b. Thus,  
35 the enlarged diameter portion 5c of the bolt 5 is held in the threaded hole 9b by the sleeve 11. The upper casing 1 is, then placed on the lower casing 2 in such a

manner that the upper end 5d of the fastening bolt 5 passes through the bolt hole 7 and protrudes therefrom. When the thread 5a of the bolt 5 is screwed into the thread 5b of the bolt hole 7, the enlarged diameter portion is pressed against the lower end face of the sleeve 11, thereby the upper casing 1 and the lower casing 2 are fastened together.

Similarly to the third embodiment, the flexural rigidity of the casing wall is increased according to the present embodiment since the diameter of the portion of the bolt hole 7 where the distance from the neutral axis of the deflection is large can be reduced.

As explained above, according to the present invention, the diameter of the bolt holes passing through the casing can be minimized. Therefore, the effective wall thickness of the casing can be kept large at the portion where the bolt holes are formed to maintain a large flexural rigidity of the casing. Further, by reducing the diameter of the bolt holes for fastening bolts, the fastening bolts can be disposed at smaller intervals, whereby a large and uniform tightening force can be obtained around the casing to minimize the deflection of the casing due to internal pressure and temperature.

Though the present invention has been described with reference to specific embodiments selected for the purpose of illustration, it should be understood that numerous modifications could be applied by those skilled in the art without departing from the basic concept and scope of the present invention.

For example, instead of the bolt head 5d in Fig. 4, a nut can be used for fastening the casing. In this case, the fastening bolt 5 is not provided with a bolt head and a screw thread is formed at the upper end of the shaft of the fastening bolt 5. A nut is engaged on the threaded upper end of the fastening bolt 5 after the bolt 5 is screwed into the threaded hole 5b in the

lower casing 2. By tightening the nut, the lower face of the nut is pressed against the flange 11f of the sleeve, whereby shaft tensile force is exerted on the fastening bolt.

5 Further, though the embodiments explained above show the case where the present invention is applied to flangeless casings, the present invention can be also applied to flanged casings in order to obtain a large and uniform fastening force of the casing by reducing the  
10 interval of the fastening bolts.

CLAIMS

1. A fastening arrangement for a split casing assembled by fastening a plurality of casing segments comprising:

5                   a first and a second casing segments assembled together by joining joint faces of the respective casing segments, said first and second casing segments are provided with bolt holes in such a manner that the bolt hole of the first casing segment and the  
10                  bolt hole of the second casing segment align with each other and, when the first and the second casing segments are assembled together, form a continuous bolt hole crossing the joint faces and extending in both casing segments and, at least the bolt hole in the first casing segment is provided with an internal screw thread;

15                  a sleeve having an external screw thread and being fitted into the bolt hole of the first casing segment by engaging the external screw thread of the sleeve with the internal screw thread of the bolt hole of the first casing segment; and

20                  a fastening bolt provided with fastening means and passing through the bolt hole of the first casing segment and the sleeve therein, wherein said fastening means abuts an end of the sleeve opposite to the joint face and, when a tensile force is exerted on the fastening bolt at the portion between the fastening means and the second casing segments, the tensile force is first transferred from the fastening bolt to the sleeve through the abutment of the fastening means and the end face of the sleeve, then transferred from the sleeve to the first casing segment through the engagement of the external screw thread of the sleeve and internal screw thread of the bolt hole and generates a fastening force for pressing the first casing segment against the  
25                  second casing segment.

30                  2. A fastening arrangement for a horizontally split type casing for a hydraulic machine in which the

casing of the hydraulic machine is assembled by fastening two casing halves comprising:

- 5            a first and a second casing halves assembled together by joining joint faces of the respective casing halves, said first and second casing halves are provided with bolt holes in such a manner that the bolt hole of the first casing half and the bolt hole of the second casing half align with each other and, when the first and the second casing halves are assembled  
10          together, form a continuous bolt hole crossing the joint faces and extending in both casing halves, said bolt holes in the first and the second casing halves are provided with internal screw threads;
- 15          a sleeve having an external screw thread and being fitted into the bolt hole of the first casing half by engaging the external screw thread of the sleeve with the internal screw thread of the bolt hole of the first casing half;
- 20          a fastening bolt provided with an external screw thread at one end for engaging the internal screw thread of the bolt hole in the second casing half and fastening means at the portion apart from said external screw thread, said fastening bolt passing through the bolt hole of the first casing half and the sleeve  
25          therein, wherein said fastening means abuts an end of the sleeve opposite to the joint face when the fastening bolt is screwed into the bolt hole in the second casing half, whereby a tensile force generated in the fastening bolt by screwing the fastening bolt into the bolt hole in the second casing half is first transferred from the fastening bolt to the sleeve through the abutment of the fastening means and the end face of the sleeve, then transferred from the sleeve to the first casing segment through the engagement of the external screw thread of the sleeve and internal screw thread of the bolt hole in the first casing half and generates a fastening force for  
30          pressing the first casing half against the second casing  
35

half.

3. A fastening arrangement as set forth in  
claim 2, wherein an enlarged diameter portion integrally  
formed on a shaft portion of the fastening bolt acts as  
the fastening element for abutting the end face of the  
sleeve.

5  
10 4. A fastening arrangement as set forth in  
claim 2, wherein an external screw thread is provided on  
a shaft portion of the fastening bolt and a nut engaging  
said external screw acts as the fastening element for  
abutting the end face of the sleeve.



FASTENING ARRANGEMENT FOR A SPLIT CASING

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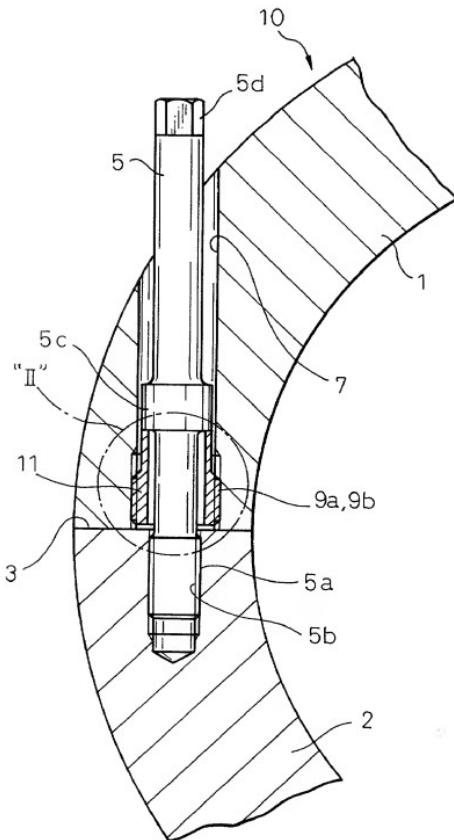
ABSTRACT OF THE DISCLOSURE

A casing of a hydraulic machine such as a gas turbine is formed as a horizontally split type flangeless casing. The flangeless casing consists of an upper casing and a lower casing joined together at joint faces and fastened by fastening bolts. The fastening bolt has a screw thread which engages the threaded hole on the joint face of the lower casing. A bolt hole having an internal screw thread and through which the fastening bolt passes is provided in the upper casing. A sleeve having an external screw thread is fitted into the bolt hole of the upper casing by engaging the external screw of the sleeve with the internal sleeve of the bolt hole.

An enlarged diameter portion is formed on a shaft of the fastening bolt at the portion where the enlarged diameter portion abuts an upper end face of the sleeve when the fastening bolt is screwed into the threaded hole in the lower casing. When the fastening bolt is tightened, the shaft tensile force of the bolt is received by the abutment of the enlarged diameter portion and the upper end face of the sleeve and, then, transferred from the sleeve to the upper casing through the engagement of the external screw thread of the sleeve and the internal screw thread of the bolt hole of the upper casing and generates the fastening force which presses the upper casing to the lower casing.

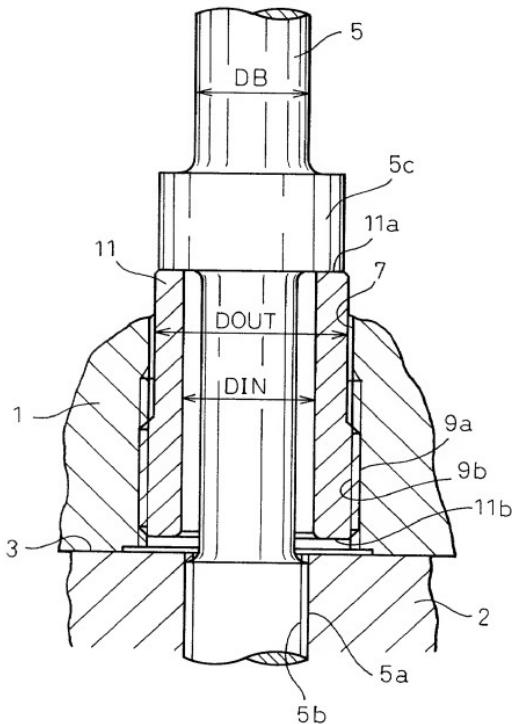
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Fig. 1



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Fig. 2



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Fig. 3A

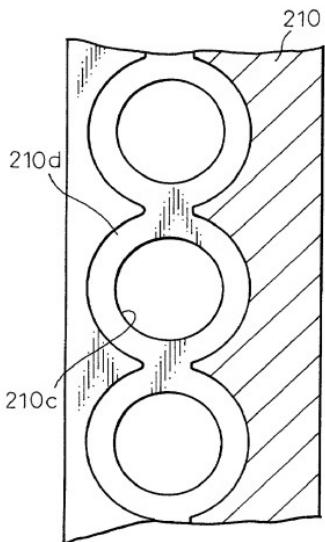
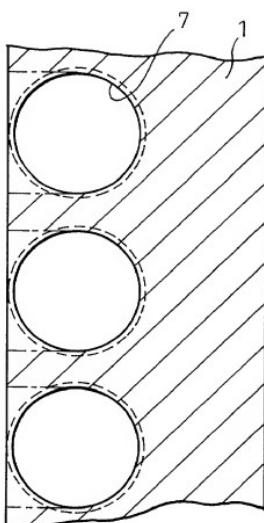


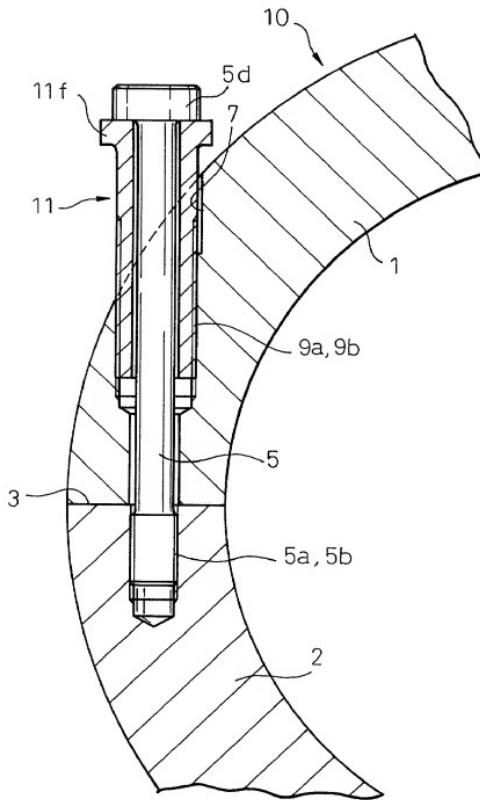
Fig. 3B



RELATED ART

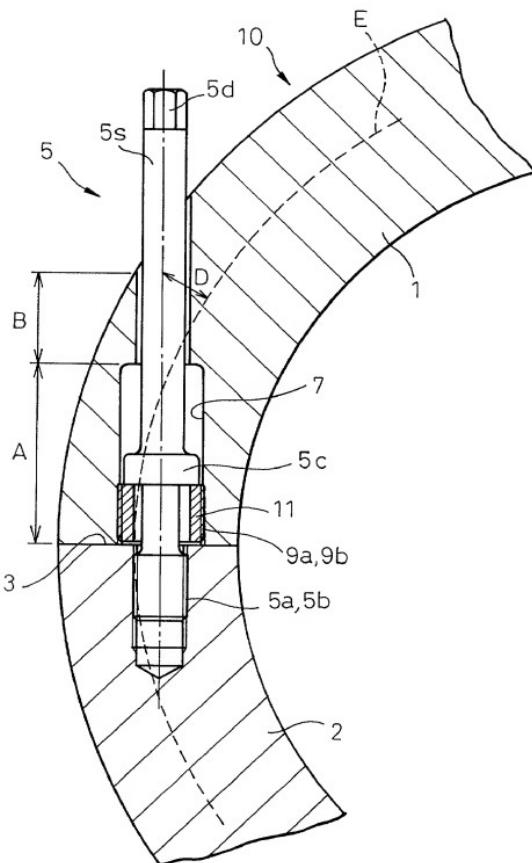
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Fig. 4



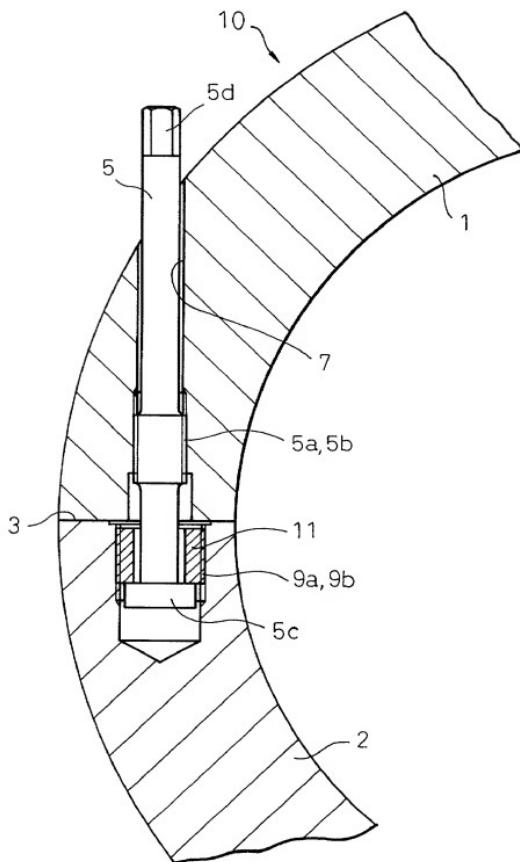
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Fig. 5



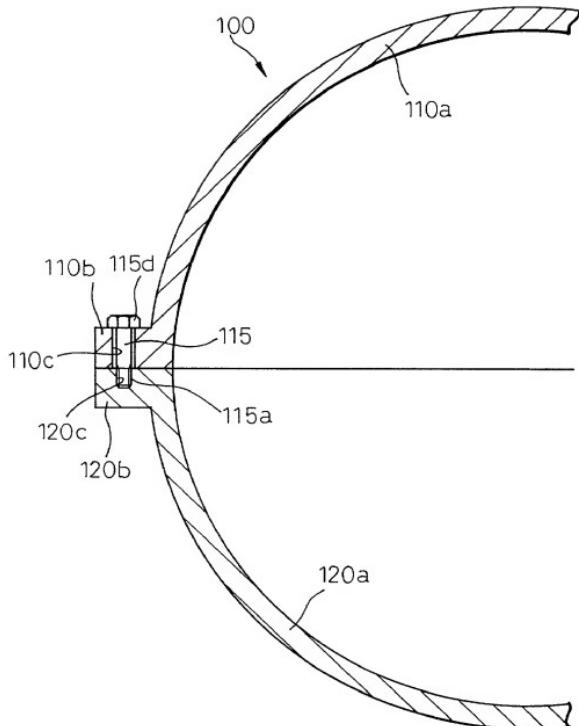
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Fig. 6



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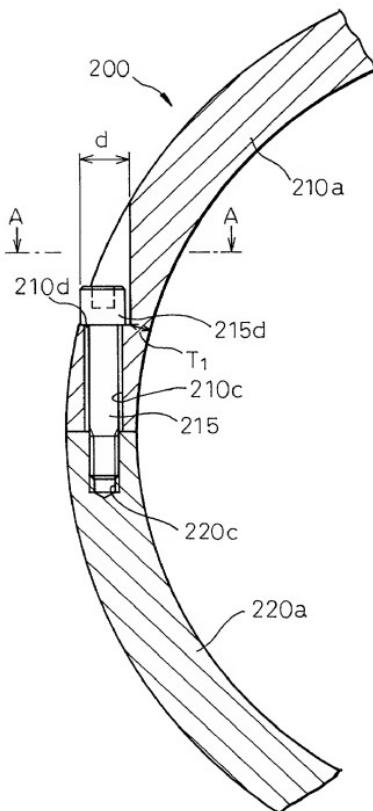
Fig. 7



RELATED ART

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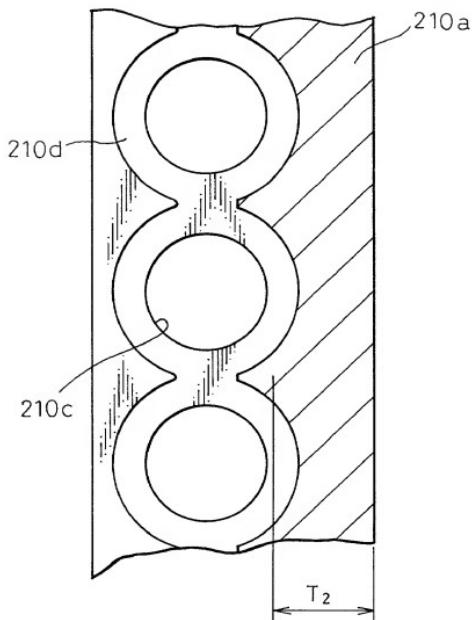
Fig. 8



RELATED ART

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Fig. 9



## Declaration and Power of Attorney For Patent Application

## 特許出願宣言書及び委任状

## Japanese Language Declaration

## 日本語宣言書

下記の氏名の発明者として、私は以下の通り宣言します。

As a below named inventor, I hereby declare that:

私の住所、私書箱、国籍は下記の私の氏名の後に記載された通りです。

My residence, post office address and citizenship are as stated next to my name.

下記の名称の発明に関して請求範囲に記載され、特許出願している発明内容について、私が最初かつ唯一の発明者（下記の氏名が一つの場合）もしくは最初かつ共同発明者（下記の名称が複数の場合）であると信じています。

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled,

## FASTENING ARRANGEMENT FOR A SPLIT CASING

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上記発明の明細書は、

本書に添付されています。

\_\_\_\_月\_\_\_\_日に提出され、米国出願番号または特許協定条

約国際出願番号を\_\_\_\_\_とし、

(該当する場合) \_\_\_\_\_に訂正されました。

the specification of which

is attached hereto.

was filed on \_\_\_\_\_

as United States Application Number or

PCT International Application Number

\_\_\_\_\_ and was amended on

\_\_\_\_\_ (if applicable).

私は、特許請求範囲を含む上記訂正後の明細書を検討し、内容を理解していることをここに表明します。

I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims, as amended by any amendment referred to above.

私は、連邦規則法典第37編第1条56項に定義されるとおり、特許資格の有無について重要な情報を開示する義務があることを認めます。

I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, Section 1.56.

## Japanese Language Declaration

(日本語宣言書)

私は、米国法典第35編119条 (a) - (d) 項又は365条 (b) 項に基づき下記の、米国以外の国の少なくとも一ヵ国を指定している特許協力条約365 (a) 項に基づく国際出願、又は外国での特許出願もしくは発明者証の出願についての外国優先権をここに主張するとともに、優先権を主張している、本出願の前に出願された特許または発明者証の外国出願を以下に、枠内をマークすることで、示しています。

### Prior Foreign Application(s)

外国での先行出願

<u>11-288549 (Pat. Appln.)</u>	<u>Japan</u>
(Number) (番号)	(Country) (国名)
(Number) (番号)	(Country) (国名)

I hereby claim foreign priority under Title 35, United States Code, Section 119 (a)-(d) or 365(b) of any foreign application(s) for patent or inventor's certificate, or Section 365(a) of any PCT International application which designated at least one country other than the United States, listed below and have also identified below, by checking the box, any foreign application for patent or inventor's certificate, or PCT International application having a filing date before that of the application on which priority is claimed.

Priority Claimed 優先権主張	
<input checked="" type="checkbox"/>	<input type="checkbox"/>
Yes はい	No いいえ
<input type="checkbox"/>	<input checked="" type="checkbox"/>
Yes はい	No いいえ

私は、第35編米国法典119条 (e) 項に基づいて下記の米国特許出願規定に記載された権利をここに主張いたします。



<u>(Application No.)</u> (出願番号)	<u>(Filing Date)</u> (出願日)
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I hereby claim the benefit under Title 35, United States Code, Section 119(e) of any United States provisional application(s) listed below.

私は、下記の米国法典第35編120条に基づいて下記の米国特許出願に記載された権利、又は米国を指定している特許協力条約365条 (c) に基づく権利をここに主張します。また、本出願の各請求範囲の内容が米国法典第35編112条第1項又は特許協力条約で規定された方法で先行する米国特許出願に開示されていない限り、その先行米国出願提出日以降で本出願書の日本国内または特許協力条約国提出日までの期間中に入手された、連邦規則法典第37編1条56項で定義された特許資格の有無に関する重要な情報をについて開示義務があることを認識しています。

<u>(Application No.)</u> (出願番号)	<u>(Filing Date)</u> (出願日)
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I hereby claim the benefit under Title 35, United States Code, Section 120 of any United States application(s), or Section 365(c) of any PCT International application designating the United States, listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT International application in the manner provided by the first paragraph of Title 35, United States Code Section 112, I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, Section 1.56 which became available between the filing date of the prior application and the national or PCT International filing date of application.

<u>(Application No.)</u> (出願番号)	<u>(Filing Date)</u> (出願日)
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Page 2 of \_\_\_\_\_

<u>(Application No.)</u> (出願番号)	<u>(Filing Date)</u> (出願日)
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Page 2 of \_\_\_\_\_

(Status: Patented, Pending, Abandoned)  
(現況: 特許許可済、係属中、放棄済)

## Japanese Language Declaration

(日本語宣言書)

委任状：私は下記の発明者として、本出願に関する一切の手続きを米特許商標局に対して遂行する弁理士または代理人として、下記の者を指名いたします。

(弁護士、または代理人の指名及び登録番号を明記のこと)

Norman F. Oblon, Registration Number 24,618; Marvin J. Spivak, Registration Number 24,913; C. Irvin McClelland, Registration Number 21,124; Gregory J. Maier, Registration Number 25,599; Arthur I. Neustadt, Registration Number 24,854; Richard D. Kelly, Registration Number 27,757; James D. Hamilton, Registration Number 28,421; Eckhard H. Kuesten, Registration Number 28,870; Robert T. Pous, Registration Number 29,099; Charles L. Gholz, Registration Number 26,395; Vincent J. Sunderdick, Registration Number 29,004; William E. Beaumont, Registration Number 30,996; Steven B. Kelber, Registration Number 30,073; Robert F. Gruse, Registration Number 27,295; Jean-Paul Lavallee, Registration Number 31,451; Stephen G. Baxter, Registration Number 32,884; Martin M. Zoltick, Registration Number 35,745; Robert W. Hahl, Registration Number 33,893; Richard L. Treanor, Registration Number 36,379; Steven P. Weirrouch, Registration Number 32,829; John T. Gookasian, Registration Number 26,142; Marc R. Labgold, Registration Number 34,651; William J. Healey, Registration Number 36,160; Richard L. Chin, Registration Number 34,305; Steven E. Lipman, Registration Number 30,011; Carl E. Schlier, Registration Number 34,426; James J. Kubaski, Registration Number 34,648; Catherine B. Richardson, Registration Number 39,007; Richard A. Neifeld, Registration Number 35,299; and J. Derek Mason, Registration Number 35,270; with full powers of substitution and revocation.

POWER OF ATTORNEY: As a named inventor, I hereby appoint the following attorney(s) and/or agent(s) to prosecute this application and transact all business in the Patent and Trademark Office connected therewith: (list name and registration number)

書類送付先

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直接電話連絡先：（名前及び電話番号）

Direct Telephone Calls to: (name and telephone number)

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第二共同発明者	Full name of second joint inventor, if any		
第二共同発明者の署名	日付	Second Inventor's signature	Date
住所	Residence		
国籍	Citizenship		
私書箱	Post Office Address		

(第三以降の共同発明者についても同様に記載し、署名すること)

(Supply similar information and signature for third and subsequent joint inventors.)